

RESEARCH LETTER

10.1002/2017GL074825

Key Points:

- A linear shallow water model is shown to be an effective means of decomposing the mean barotropic transport from a high-resolution, eddying model of the North Atlantic based on the vertically averaged horizontal momentum equations
- The potential energy, mean flow advection, and eddy momentum flux terms all contribute to the mean barotropic transport of the Gulf Stream and its extension, including the northwest corner and the Mann Eddy
- Mean flow advection is found to play an important role in the interaction between the circulation and the continental slope

Supporting Information:

- Supporting Information S1

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Citation:

Wang, Y., Claus, M., Greatbatch, R. J. & Sheng, J. (2017). Decomposition of the mean barotropic transport in a high-resolution model of the North Atlantic Ocean. *Geophysical Research Letters*, 44, 11,537–11,546. <https://doi.org/10.1002/2017GL074825>

Received 5 JUL 2017

Accepted 1 NOV 2017

Accepted article online 6 NOV 2017

Published online 20 NOV 2017

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Decomposition of the Mean Barotropic Transport in a High-Resolution Model of the North Atlantic Ocean

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Abstract We show how a barotropic shallow water model can be used to decompose the mean barotropic transport from a high-resolution ocean model based on the vertically averaged momentum equations. We apply the method to a high-resolution model of the North Atlantic for which the local vorticity budget is both noisy and dominated by small spatial scales. The shallow water model acts as an effective filter and clearly reveals the transport driven by each term. The potential energy (joint effect of baroclinicity and bottom relief) term is the most important for driving transport, including in the northwest corner, while mean flow advection is important for driving transport along f/H contours around the Labrador Sea continental slope. Both the eddy momentum flux and the mean flow advection terms drive significant transport along the pathway of the Gulf Stream and the North Atlantic Current.

1. Introduction

The Gulf Stream and its extensions play an important role in the Northern Hemisphere climate (Minobe et al., 2008; O'Reilly et al., 2016; Scaife et al., 2014), because of its massive volume transport and associated redistribution of heat and salinity (Böning et al., 2016; Trenberth & Caron, 2001). After the Gulf Stream detaches from the shelf break at Cape Hatteras, its volume transport increases dramatically up to about 150 Sverdrup (Sv) (Fuglister, 1963). This increase in transport has been attributed to the presence of the Northern Recirculation Gyre on its north side and the Worthington Gyre on its south side (Hogg, 1992; Hogg et al., 1986; Worthington, 1976). The Gulf Stream reattaches to the bottom slope at the southern tip of the Grand Banks of Newfoundland and the Newfoundland Ridge. Its main branch follows the slope of the Newfoundland Shelf northward as the North Atlantic Current (NAC), before it turns sharply eastward at the northwest corner, heading toward Europe.

The dynamics of the northwest corner (centered at about 50°N, 45°W) (Lazier, 1994) and the recirculation gyres associated with the Gulf Stream and its extensions are not fully understood, and general circulation models have trouble reproducing these features of the circulation. Typically, for example, the northwest corner is missing due to the misplaced NAC (see Delworth et al., 2012; Drews et al., 2015; Flato et al., 2013; Griffies et al., 2015), leading to the so-called “cold bias” that, in turn, can be detrimental to the representation of low-frequency variability in models (Drews & Greatbatch, 2016, 2017) and also to the overlying atmosphere in coupled models (Keeley et al., 2012; Scaife et al., 2011). Furthermore, the region of the Mann Eddy (centered at about 42°N, 46°W) is suggested to be a pivotal point in modulating variability of the Atlantic Meridional Overturning Circulation (Tulloch & Marshall, 2012).

There has long been discussion on the dynamics driving the recirculation gyres. It has been suggested that the deep circulation plays an important role in their dynamics through the bottom pressure torque and associated bottom vortex stretching (Greatbatch et al., 1991; Holland, 1973; Zhang & Vallis, 2007). Recirculation gyres have also been modeled using extensions to a stratified ocean of the Fofonoff (1954) model (Greatbatch, 1987; Marshall & Nurser, 1986). In these models, the eddy fluxes provide a weak forcing while it is the advection by the mean flow, in particular the advection of mean vorticity in the time-averaged vorticity equation, that shields the recirculation gyres from the influence of the eastern boundary and allows the transport to exceed the Sverdrup transport. Hogg and Stommel (1985) had earlier noted that closed potential vorticity contours can occur beneath the Gulf Stream due to the tilt of the isopycnals and the underlying topography (see also Greatbatch & Zhai, 2006) and that transient eddies can drive large transports within these contours. More recently, Greatbatch et al. (2010) have estimated that the transport driven by the

eddy momentum fluxes alone is comparable to the observed total transport in the Gulf Stream and North Atlantic Current region. In that paper, the surface eddy momentum fluxes were derived from satellite altimetry observations. However, a vertical profile for the eddy momentum fluxes had to be assumed to calculate the vertical integral of the fluxes that is difficult to verify given the limited observations. One of the aims of the present study is to assess the importance of the eddy momentum fluxes, compared to other drivers for vertically integrated transport, in a high-resolution ocean model.

Traditionally, the vertically integrated (barotropic) gyre transport in the ocean has been understood in terms of the vorticity equation derived from either the vertically integrated or the vertically averaged momentum equations (see, for example, Bell, 1999 and Yeager, 2015). The former approach (see equation (S24) in the supporting information), based on vortex stretching of the water column, takes the flat-bottom Sverdrup transport (equation (S25)) implied by the surface wind stress as its reference point, and the effect of variable bottom topography enters by means of the bottom pressure torque (see Holland, 1973, for an early example). On the other hand, when considering the vorticity equation derived from the vertically averaged momentum equations (equation (S21) in the supporting information), the reference is the topographic Sverdrup transport for a uniform density ocean (equation (S22)). The effect of density stratification is included by means of the joint effect of baroclinicity and bottom relief (JEBAR) term (see Mertz & Wright, 1992, for a detailed discussion of JEBAR), an approach dating back to Sarkisyan and Ivanov (1971). Greatbatch et al. (1991) exploited these two different approaches in order to suggest a decomposition of the gyre transport into its different components and illustrated their decomposition for the North Atlantic using the diagnostic model of Mellor et al. (1982). Bell (1999) and Yeager (2015) have discussed both approaches applied as model diagnostics, the former focusing on the North Atlantic and the representation of the Gulf Stream in models, and latter showing how the same approach can be used to provide a decomposition for the meridional overturning circulation in models. Neither Bell (1999) nor Yeager (2015) used models that included eddies and were therefore unable to say anything about the transport that is driven by the eddy momentum fluxes.

In order to infer the transport driven by the eddy momentum fluxes, Greatbatch et al. (2010) used a barotropic, linear shallow water model driven by forcing terms that were specified in the horizontal momentum equations. The barotropic model solves for the vertically averaged (barotropic) velocity, and the forcing terms were derived by vertically averaging the momentum flux convergence implied by the satellite-derived surface eddy momentum fluxes based on the assumed vertical profile. Their approach is therefore based on the vertically averaged, rather than the vertically integrated, momentum equations. In the present study, we extend this approach to include, additionally, forcing terms associated with mean flow advection, the potential energy (which leads to the JEBAR term in the vorticity equation), and direct wind forcing (as for a uniform density ocean) (see equation (S11)). A detailed derivation of the forcing terms is given in the supporting information. The forcing terms are, in turn, derived from a high-resolution ocean model that includes mesoscale eddies. We show that the local vorticity budget in the model is quite noisy and is dominated by small spatial scales from which it is difficult to infer the relative importance of the different forcing terms. Dynamically computing the implied transport using the shallow water model acts as an effective filter enabling the transport stream function from the high-resolution model to be decomposed into its separate parts.

The high-resolution ocean model used here is the VIKING20 configuration (Behrens, 2013). VIKING20 has the advantage that it captures the Gulf Stream, NAC, and their associated recirculation gyres without data assimilation (see Mertens et al., 2014, and Breckenfelder et al., 2017, for a detailed assessment of the performance of VIKING20). Section 2 presents the four forcing terms and discusses the setup of the linear shallow water model used to compute the transport driven by each forcing term. Results for the mean transport averaged over 50 years (1960–2009) are shown and discussed in section 3. A summary and discussion are given in section 4.

2. Methods

VIKING20 is a two-way nested ocean model configuration that consists of a high-resolution ($1/20^\circ$) component (referred to as the nest in the following), covering the northern North Atlantic (from $\sim 30^\circ\text{N}$ to 85°N) that is embedded within a global component of roughly $1/4^\circ$ horizontal resolution (referred to as the base). Both components are composed of the Nucleus for European Modelling of the Ocean (NEMO)

(Madec, 2008), using the Océan PARallélisé system (OPA) for ocean circulation, and the Louvain-la-Neuve Ice Model version 2 (LIM2) for sea ice. The two-way nesting is accomplished with the help of the Adaptive Grid Refinement In Fortran (AGRIF) system (see Behrens, 2013, and Böning et al., 2016, for the details). After a 30 year spin-up of the base component alone, VIKING20 was integrated from 1948 to 2009 using the Coordinated Ocean-Ice Reference Experiment 2 atmospheric forcing (Large & Yeager, 2009). Output produced by the nest component of VIKING20 during the period of 1960–2009 is used in this study to calculate the forcing terms for the vertically and time-averaged horizontal momentum equations. It should be noted that the separation between the mean and the perturbation velocity is carried out each year separately, following Rieck et al. (2015). As such, the mean flow advection forcing also includes a rectified contribution from the interannual variability.

To compute the barotropic transport driven by each of the forcing terms, we use a linear, barotropic shallow water model (SWM) that is run to steady state. In steady state, the equations governing the SWM are

$$\begin{aligned} -fv &= Z - \frac{1}{\rho_0 a \cos \theta} \frac{\partial p_b}{\partial \lambda} - \frac{ru}{H} + F_x \\ fu &= M - \frac{1}{\rho_0 a} \frac{\partial p_b}{\partial \theta} - \frac{rv}{H} + F_y \\ 0 &= \frac{1}{a \cos \theta} \left[\frac{\partial Hu}{\partial \lambda} + \frac{\partial \cos \theta H v}{\partial \theta} \right] \end{aligned}$$

where each of the four forcing terms in turn is denoted as (Z, M) , where Z is the zonal component and M is the meridional component. It should be noted that the free surface variable in the SWM should be interpreted as the bottom pressure, p_b ; a is the radius of the Earth; (λ, θ) are longitude and latitude; u and v are vertically averaged velocities in the eastward and northward directions, respectively; H is the ocean bottom depth; r is a linear bottom friction coefficient; and (F_x, F_y) denotes a horizontal Laplacian viscosity term with lateral eddy viscosity coefficient given by A_h (see the supporting information for the detailed expression).

The forcing terms, (Z, M) , are computed from the output of the nest component of VIKING20 for each year separately and then averaged over all years to provide the forcing for the SWM. The formulation of (Z, M) in the four cases is given below (the detailed derivation is given in the supporting information), where an overbar denotes a time average over a single year (following Rieck et al., 2015) and $\langle \rangle$ a vertical integral from $z = -H$ (corresponding to the ocean bottom) to $z = 0$ (the ocean surface):

1. The potential energy term:

$$\begin{aligned} Z &= -\frac{1}{Ha \cos \theta} \left[\frac{\partial}{\partial \lambda} \left\langle g \frac{(\rho - \rho_m)}{\rho_0} z \right\rangle \right] \\ M &= -\frac{1}{Ha} \left[\frac{\partial}{\partial \theta} \left\langle g \frac{(\rho - \rho_m)}{\rho_0} z \right\rangle \right] \end{aligned}$$

where ρ represents the in situ density and ρ_m represents the horizontally averaged mean density.

2. Mean flow advection:

$$\begin{aligned} Z &= -\frac{1}{Ha \cos \theta} \left[\frac{\partial \langle \bar{u} \bar{u} \rangle}{\partial \lambda} + \frac{\partial \cos \theta \langle \bar{u} \bar{v} \rangle}{\partial \theta} \right] \\ M &= -\frac{1}{Ha \cos \theta} \left[\frac{\partial \langle \bar{v} \bar{u} \rangle}{\partial \lambda} + \frac{\partial \cos \theta \langle \bar{v} \bar{v} \rangle}{\partial \theta} \right] \end{aligned}$$

3. Eddy momentum flux:

$$\begin{aligned} Z &= -\frac{1}{Ha \cos \theta} \left[\frac{\partial \langle \bar{u}' \bar{u}' \rangle}{\partial \lambda} + \frac{\partial \cos \theta \langle \bar{u}' \bar{v}' \rangle}{\partial \theta} \right] \\ M &= -\frac{1}{Ha \cos \theta} \left[\frac{\partial \langle \bar{u}' \bar{v}' \rangle}{\partial \lambda} + \frac{\partial \cos \theta \langle \bar{v}' \bar{v}' \rangle}{\partial \theta} \right] \end{aligned}$$

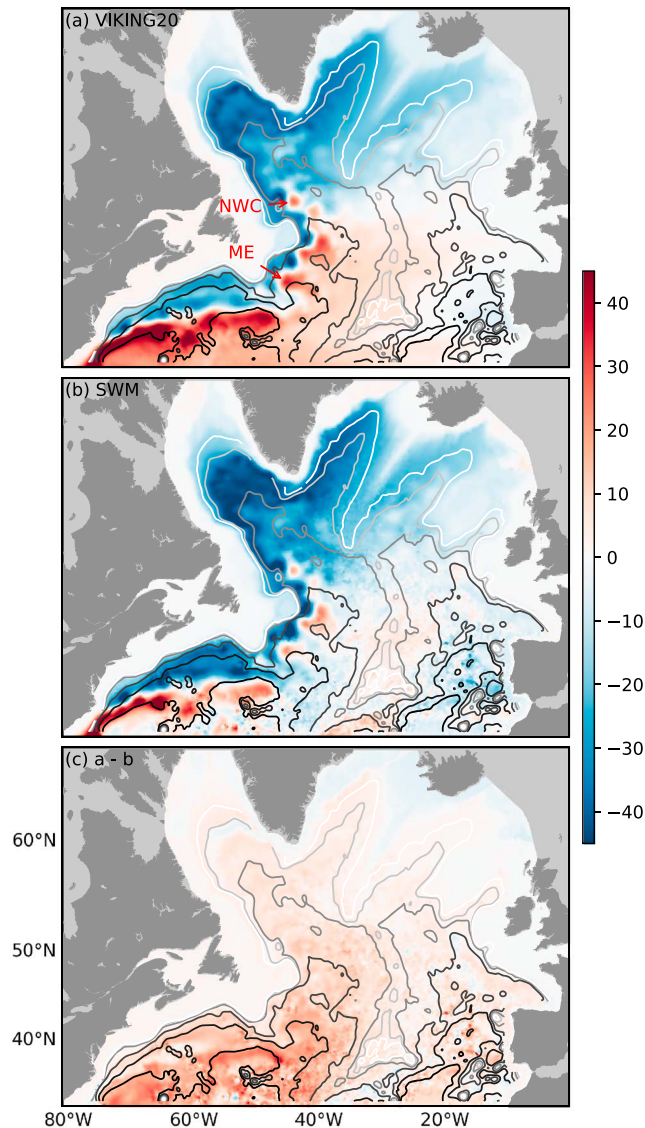


Figure 1. Model-computed 50 year mean barotropic transport (color shading in units of Sverdrups) for (a) the VIKING20 nest, (b) the sum of the four cases computed by the SWM, and (c) a–b. The lines are f/H contours of 17, 20, 25, 35, 45, and 55 in units of $10^{-9} \text{ s}^{-1} \text{ m}^{-1}$, which are smoothed using a Gaussian filter with a standard deviation of 0.5° in latitude and longitude. The locations of the northwest corner (NWC) and Mann Eddy (ME) are shown (Figure 1a).

4. The wind stress term:

$$Z = \frac{\overline{\tau_x^x}}{\rho_0 H}$$

$$M = \frac{\overline{\tau_x^y}}{\rho_0 H}$$

The SWM in this study is very similar to the model described by Greatbatch et al. (2010) and is set up for the model domain covered by the high-resolution nest component of VIKING20. The model uses a staggered latitude/longitude C-grid with a horizontal resolution of $1/20^\circ$ covering the North Atlantic between 85°W to 5°E and from 31°N to 67°N . The bottom topography is interpolated from that of the VIKING20 nest component to the SWM grid. To keep the model stable and restrict noise, a linear bottom friction coefficient with $r = 5 \times 10^{-4} \text{ m s}^{-1}$ and Laplacian horizontal viscosity coefficient $A_h = 150 \text{ m}^2 \text{ s}^{-1}$ are applied. While there is some sensitivity to the choice of these values, the stream function computed from the SWM, when all four forcings are used together, is close to that from VIKING20, as we show in Figure 1 (discussed in detail later), suggesting that these values effectively mimic the dissipation in VIKING20 (which, in any case, are not part of the available model output). In addition, to inhibit topographic instability associated with the steep and rough topography (Killworth, 1987) on the high-resolution SWM grid, a 3-by-3 running average filter is applied to smooth regions with water depth less than 1,000 m. Note that we want to preserve the topography in the deep ocean as close as possible to that of the nest component of VIKING20 since this study focuses on the large-scale barotropic transport in the open ocean rather than on the shelf. In addition, Hudson Strait, Davis Strait, Denmark Strait, the Faroe Bank Channels, the English Channel, and the Strait of Gibraltar are all closed in the model.

Unlike the VIKING20 nest, the lateral boundaries of the SWM are closed, since we do not attempt to decompose the open boundary forcing for the VIKING20 nest component according to each forcing term. Since there are f/H contours that enter the model domain at the southern boundary, transport driven by each forcing term outside the SWM domain (which is the same as that of the VIKING20 nest) is not taken care of by our model solution and this indeed has an impact on the computed barotropic transport, as we discuss later. While this is a disadvantage of our method as applied to VIKING20, the problem would

not arise if the southern boundary of the nest extended south of the equator since then the southern boundary of the SWM domain would not cross f/H contours.

3. Results

Figure 1a presents the total barotropic transport computed directly from VIKING20 within the region of the VIKING20 nest, and Figure 1b presents the sum of the barotropic transport from the SWM driven by each of the four forcing terms separately (note that since the SWM is linear, this is the same as the transport driven by all four terms together). The barotropic transport from the VIKING20 nest (Figure 1a) depicts a well-developed northern recirculation gyre south of Atlantic Canada, and recirculation gyres associated with the North Atlantic Current, including the anticyclonic Mann Eddy centered at 42°N , 46°W and the northwest corner near 50°N , 45°W . The recirculation gyres in the SWM are at the same locations and of similar strengths

to those in the VIKING20 nest, which indicates that our linear decomposition method is able reproduce their dynamics from VIKING20. Nevertheless, the combined barotropic transport from the SWM is weaker in the subtropical gyre and a bit stronger in the subpolar gyre. The difference, as shown in Figure 1c, is mostly associated with the closed southern boundary in the SWM; indeed, the difference in the barotropic transport is generally anticyclonic, following the f/H contours. It is also possible that some of the difference is related to the different friction parameterizations used in the SWM and VIKING20. Nevertheless, the unexplained barotropic transport does not exhibit the recirculation gyres or quasi-stationary eddies along the Gulf Stream and the North Atlantic Current, which implies that the dynamics of these recirculation gyres are primarily explained by the four forcing terms specified within the SWM domain.

Figure 2 shows the 50 year mean barotropic transport driven by the potential energy (PE), mean flow advection, eddy momentum flux, and the wind stress terms (here the wind-driven transport for an ocean of uniform density), and the ratio of their contributions to the total explained barotropic transport from the SWM. The PE term plays a dominant role over most parts of the model domain, especially in the subpolar gyre, the Northern Recirculation Gyre, and the Gulf Stream separation region, including the Worthington Gyre, consistent with previous studies (e.g., Greatbatch et al., 1991; Myers et al., 1996). The PE term also plays the primary role along the path of the Gulf Stream, where it is complemented by the mean flow advection and eddy momentum flux terms. The mean flow advection term also drives considerable barotropic transport around the western subpolar gyre associated with the recirculating boundary current around the Labrador Sea and Irminger Sea (Fischer et al., 2015; Lavender et al., 2000). The mean flow advection and, to some extent, the eddy momentum flux terms, drive a series of recirculations along the path of the Gulf Stream and the North Atlantic Current, including in the northwest corner, not unlike the eddy-driven transport inferred for this region by Zhai et al. (2004). In the northwest corner, the mean flow advection term predominantly drives the anticyclonic mesoscale recirculation centered at 50°N, 45°W, but with some role for the PE and eddy momentum flux terms. For the Mann Eddy the mean flow advection/eddy momentum flux and PE terms are dominant over the eastern and western halves, respectively. This implies that all three dynamical processes are working together to shape this semipermanent anticyclonic eddy. The location of the Mann Eddy and the adjacent North Atlantic Current is observed to migrate over 200 km (Meinen, 2001), suggesting variability in the relative importance of these terms over time.

Figure S1 in the supporting information shows the local vorticity budget diagnosed from VIKING20 and based on equation (S21). It should be noted that the plotted fields have been smoothed to reduce noise. The plotted fields nevertheless exhibit mostly small-scale features, and it is difficult to infer the relative importance of the different forcing terms. Similar plots in Bell (1999) and Yeager (2015) are more informative, but it should be noted that the models they used have much coarser resolution with much less detailed bottom topography (a major source of noise) than is carried by VIKING20. An advantage of our method is that the SWM effectively integrates the forcing terms to provide transport fields (without smoothing) that not only closely resemble that in VIKING20 (Figure 1) but also provide an effective decomposition of the transport in VIKING20 into its constituent parts (Figure 2). Furthermore, as we noted earlier, the southern boundary of the VIKING20 nest would be much less troublesome if it was located either at or south of the equator. A good example, illustrating the power of our method, is provided by the eddy momentum flux forcing. From Figure S1, this appears weak and much less important than implied by Figure 2. Nevertheless, some useful information can be gained from Figure S1. The general tendency (although not universal) for the JEBAR term to balance the advection of planetary vorticity is consistent with the dominance of the PE term for explaining the transport in VIKING20 (Figure 2). Furthermore, it is seen that the mean flow advection term is most important in the region of the East Greenland Current and it appears that this region plays a role in driving the recirculation gyre around the rim of the Labrador Sea that can be seen in Figure 2b.

Compared to the barotropic transport driven by the eddy momentum fluxes in Greatbatch et al. (2010) using satellite-altimetry-derived forcing, the SWM, using the forcing derived from the output of the VIKING20 nest, generates a very similar pattern but less magnitude. As noted earlier, Greatbatch et al. (2010) had to assume a vertical profile for the eddy momentum fluxes and, as noted by these authors, the more surface trapped the profile, the less the transport that is driven by these terms. Since the eddy momentum fluxes derived from the VIKING20 nest have a similar magnitude at the surface to those seen in the altimeter data (not shown), the explanation for the reduced transport computed here is almost certainly that the vertical profile of the fluxes in the model is surface intensified (see Figure S2 in the supporting information), rather than linear, as

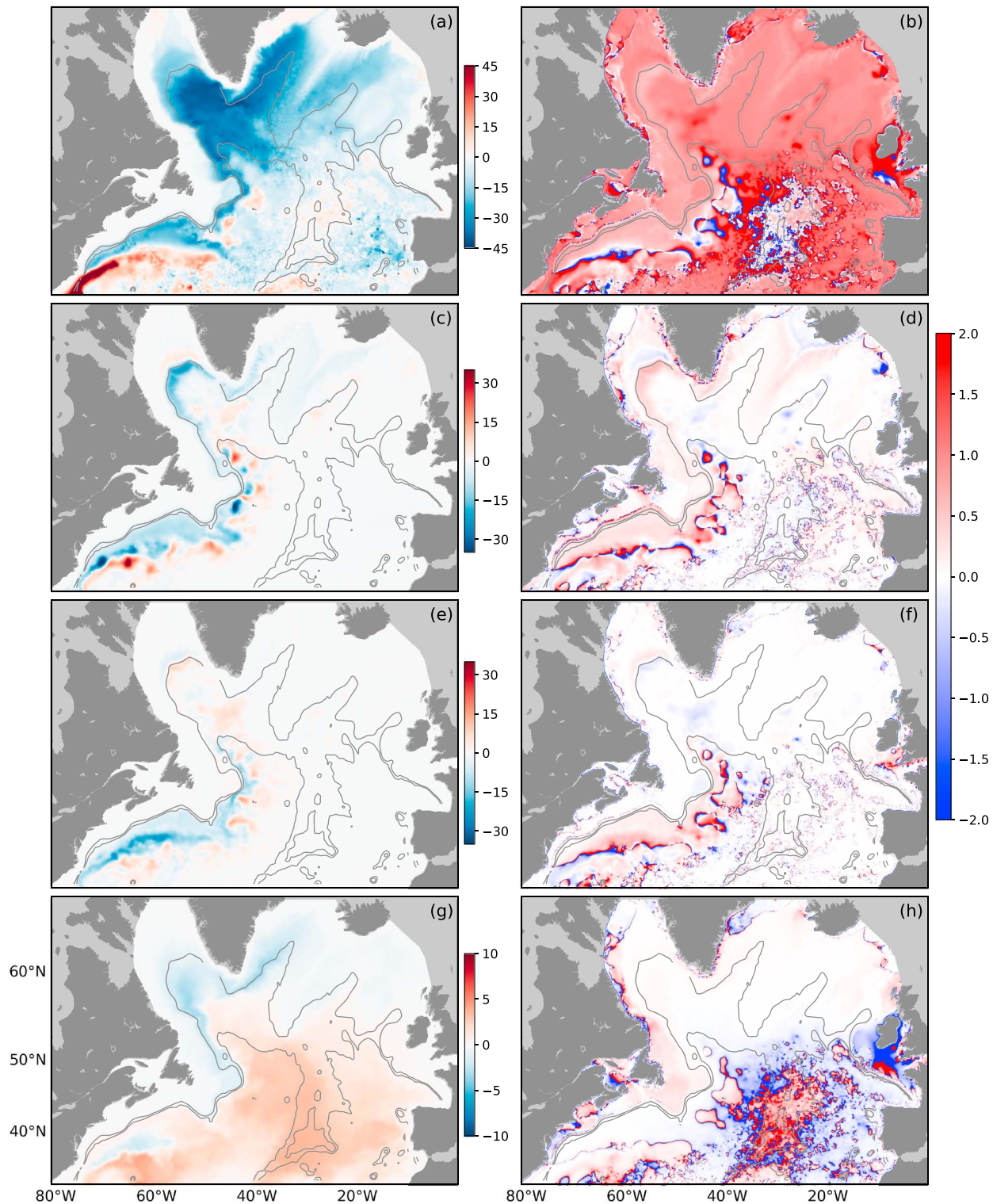


Figure 2. Model-computed 50 year mean barotropic transport (color shading in units of Sverdrups) driven by (a) the PE (JEBAR), (c) mean flow advection, (e) eddy momentum flux, and (g) wind stress terms. Note that the color coding is not the same in all panels. (b, d, f, and h) The ratio of the corresponding barotropic transport to the total barotropic transport (as shown in Figure 1b). The contours are f/H contours of 30 and 45 in units of $10^{-9} \text{ s}^{-1} \text{ m}^{-1}$, which are smoothed using a Gaussian filter with a standard deviation of 0.5° in latitude and longitude.

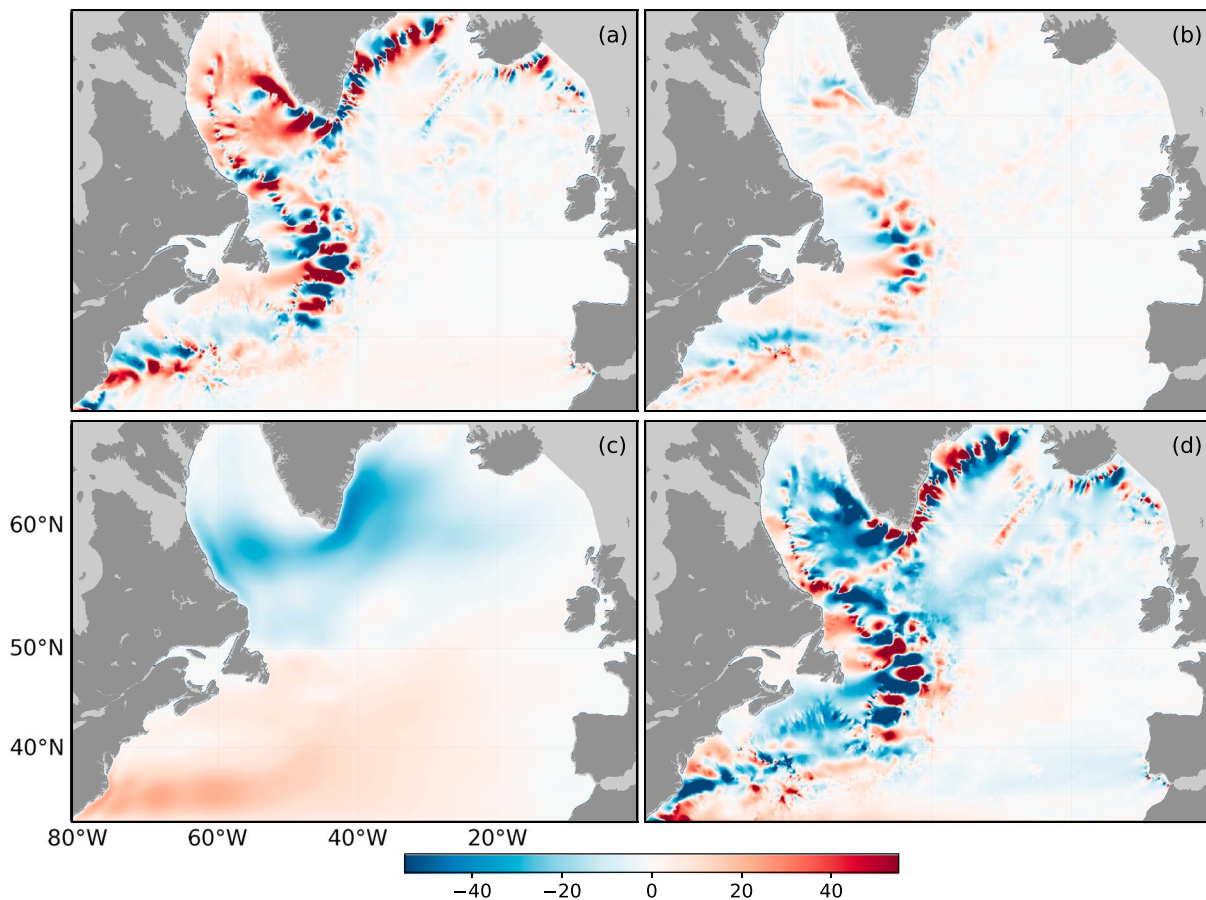


Figure 3. Model-computed 50 year mean barotropic transport (color shading in units of Sverdrups) for the flat bottom case driven by (a) mean flow advection, (b) eddy momentum flux, (c) wind stress, and (d) the part that is estimated to be driven by bottom pressure torque.

assumed by Greatbatch et al. (2010). Furthermore, the vertical integral of the vertical profile shown in Figure S2 has about 25% the magnitude of the corresponding linear profile assumed by Greatbatch et al. (2010), similar to the reduction in the magnitude of the transport that is driven by these terms (Figure 2c) compared to that reported by Greatbatch et al. (2010).

The barotropic transport that is directly driven by the surface wind stress within the SWM domain (Figure 2g) is weak but, nevertheless, has a role to play over the Mid-Atlantic Ridge south of the Charlie-Gibbs Fracture zone (Figure 2h). Note that the wind-driven transport presented here is the wind-forced response of a uniform density ocean which, as noted by Greatbatch et al. (1991), is very different in the North Atlantic from that of the flat-bottom Sverdrup transport (compare Figures 2g and 3c to see this comparison directly). This is because the presence of the Mid-Atlantic Ridge causes the f/H contours to exhibit large latitudinal excursions. Furthermore, our diagnosis of the response to this term is affected by the closed southern boundary and is missing transport that would otherwise propagate into the SWM domain from the south along the western side of the mid-Atlantic ridge and also near the eastern boundary. For example, a comparison with Figure 2a in Greatbatch et al. (1991) shows much more transport in the subtropical gyre region, west of the Mid-Atlantic Ridge, than can be seen in Figure 2g.

We can also decompose the barotropic transport following equation (S24) in the supporting information. Since (S24) is the vorticity balance for the vertically integrated, as distinct from the vertically averaged, momentum equations, the forcing terms are the eddy momentum flux, mean flow advection, and wind stress terms given in section 2 but now multiplied by the local depth H , and the SWM is run using a uniform depth, here taken to be 4,000 m with the lateral eddy viscosity is reduced to $2 \text{ m}^2 \text{ s}^{-1}$. Note that using the value of $150 \text{ m}^2 \text{ s}^{-1}$ reduces the amplitude shown but does not affect the spatial pattern, and also that integrating the

forcing terms directly along lines of latitude, following (S24), leads to a very noisy solution from which it is hard to extract the signal. To estimate the barotropic transport driven by the bottom pressure torque (Figure 3d), we take the transport stream function from VIKING20 shown in Figure 1a and subtract the parts that are associated with the eddy momentum fluxes (Figure 3a), mean flow advection (Figure 3b), and surface wind stress (Figure 3c), the latter corresponding to the flat-bottom Sverdrup transport given by equation (S25) (modified by the lateral mixing as in the model of Munk, 1950). From Figure 3, we see that the implied transport driven by the bottom pressure torque is strongly influenced by the mean flow advection and eddy momentum flux contributions, especially the former. Indeed, it is clear that there is a lot of cancellation between Figures 3a and 3d suggesting that the mean flow advection has a big influence on how the circulation interacts with the sloping bottom topography in the model, appearing, in fact, to be more important than the spreading of newly formed dense water masses. If the latter were important, then the transport driven by the bottom pressure torque would be dominated by the difference between the VIKING20 stream function and the component driven by the surface wind stress (Figure 3c). Clearly, this is not the case.

4. Summary and Discussions

In this study, the mean barotropic transport in the North Atlantic Ocean has been diagnosed using a shallow water model (SWM) driven by forcing terms derived from the high-resolution component of a nested ocean circulation model configuration, VIKING20. By this method, the mean barotropic transport over the period of 1960–2009 simulated by VIKING20 (without data assimilation) can be attributed to four forcing terms in the vertically averaged momentum equation: the eddy momentum flux, mean flow advection, potential energy (PE), and wind stress forcing for an ocean of uniform density (Figure 2). We have seen that the local vorticity budget is noisy and characterized by small spatial scales (Figure S1) from which it is difficult to infer the relative importance of the different forcing terms. For example, the eddy momentum flux terms appear to be unimportant in Figure S1, yet are a significant contributor to the transport of the Gulf Stream and its recirculations. Indeed, the SWM approach adopted here offers a powerful tool for diagnosing the transport output from high-resolution ocean models and is an effective alternative when analyzing models that include eddies to the approaches adopted to Bell (1999) and Yeager (2015).

Regarding the four forcing terms, the PE term is the primary forcing, including in the northwest corner region east of Newfoundland where models have great difficulty simulating the circulation (see Delworth et al., 2012; Drews et al., 2015; Flato et al., 2013; Griffies et al., 2015) and the recirculation gyres associated with the Gulf Stream Extension, consistent with previous work (e.g., Greatbatch et al., 1991; Zhang & Vallis, 2007). Both the eddy momentum flux and the mean flow advection terms play a significant role in the Gulf Stream region and its extensions, including the North Atlantic Current, and the mean flow advection is found to be an important driver for transport around the rim of the Labrador Sea (this is the recirculation gyre noted by Lavender et al., 2000, based on drifter data). The transport driven by the eddy momentum fluxes shows a very similar pattern to the transport stream function derived in a previous study using eddy momentum fluxes derived from satellite data (Greatbatch et al., 2010) apart from the lower amplitude, which we attribute to the vertical profile of eddy momentum fluxes assumed in that study; in the VIKING20 nest the eddy momentum fluxes are more surface intensified (Figure S2). Interestingly, in addition to PE forcing (i.e., JEBAR), both the eddy momentum fluxes and mean flow advection play a role in driving the Gulf Stream recirculation gyres either side of the Gulf Stream Extension (Hogg, 1992). The fact the eddy momentum fluxes are important shows that unlike in the theories of Marshall and Nurser (1986) and Greatbatch (1987), the eddy forcing of these gyres is not “weak”. The theory in those papers depends on the mean flow advection term playing a major role, and it is interesting that some role for this term is, indeed, found. In general, the wind stress forcing (which leads to the response for a uniform density ocean) has a relatively minor contribution that arises from the blocking of the f/H contours by the Mid-Atlantic Ridge (Figure 1c) (Greatbatch et al., 1991) and the closed southern boundary for our SWM.

This study explicitly illustrates the dynamics governing the recirculation gyres associated with the Gulf Stream and North Atlantic Current, including the northwest corner, which are not well understood. It is demonstrated that the northwest corner is primarily driven by the combination of the PE and mean flow advection terms with some role for the eddy momentum fluxes. The role of the PE forcing is anticipated given the impact of the flow-field correction in alleviating the cold bias in Drews et al. (2015), since the correction assumes that a diagnostic calculation, in which the density field is specified, is capable of reproducing the

northwest corner in a model. Another example is the Mann Eddy, which is a semipermanent anticyclonic eddy that is observed to migrate sometimes over a distance of 200 km (Meinen, 2001). Figure 2 suggests that the east/west side of the Mann Eddy is primarily driven by the mean flow advection and eddy momentum flux/PE terms. This explains the eastward shift in the position of the Mann Eddy in the study using only the eddy momentum flux forcing by Greatbatch et al. (2010), and may also explain the challenge for a $1/4^\circ$ horizontal resolution model to reproduce the eastern branch of the Mann Eddy (see Figure 5a in Urrego-Blanco & Sheng, 2012).

It is still challenging for numerical models to replicate many observed recirculation gyres, especially for climate models that trade off resolution and dynamics for efficiency, which can be significantly detrimental to the model veracity (e.g., the cold bias). Numerical corrections, such as those described by Drews et al. (2015), turn out to be one possible way to improve the model performance, while the lack of knowledge on dynamics driving those recirculation gyres imposes difficulties. The importance of the PE term in the dynamics of the northwest corner is consistent with previous studies (e.g., Zhang et al., 2011). Nevertheless, a new and surprising result is the influence that the mean flow advection has on the interaction between the circulation and the sloping bottom topography, i.e., the bottom pressure torque (see Figure 3). This suggests a feedback between the circulation in the continental slope region and the mean flow advection that might well contribute to the difficulties models have with, for example, Gulf Stream separation and the northwest corner. We suggest that the method presented here, using a linear shallow water model, is an effective tool with which to diagnose the drivers for transport in high-resolution ocean models, including models that do not exhibit a northwest corner or a correct Gulf Stream separation. Such diagnoses are needed in order to disentangle the different types of feedback operating in these models.

Acknowledgments

We are grateful to three reviewers for their constructive comments on the manuscript. These comments have led to considerable improvements. Y.W. is grateful for funding support from the NSERC CREATE Transatlantic Ocean System Science and Technology (TOSST) grant and for the opportunity to spend 4 months at GEOMAR. J.S. is funded by the MEOPAR and NSERC. Support is also acknowledged from the German Ministry for Education and Research (BMBF) through MiKlip2, sub-project 01LP1517D (ATMOS-MODINI). M.C. is grateful for funding support from the Deutsche Forschungsgemeinschaft through the Sonderforschungsbereich 754 "Climate-Biogeochemistry Interactions in the Tropical Ocean". R.J. G. is also grateful for continuing support from GEOMAR. Data shown in this paper are available at data.geomar.de.

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